

# REVIEW OF CRYOGENIC TECHNIQUE FOR AUTOMOTIVE APPLICATIONS

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## ABSTRACT

*Cryogenics are efficient thermal storage media which, when used for Automotive purposes, offer significant advantages over Electrochemical battery sciences, both in performance and economy. An Automotive propulsion concept is presented which use liquid N<sub>2</sub> as the Working fluid for an open Rankine cycle. The principle of performance is like that of a steam engine, except there is no heating involved. Liquid N<sub>2</sub> (nitrogen) is Pressurized and then evaporate in a heat exchanger by the atm. (atmospheric) temperature of the surrounding air. The resulting high - pressure nitrogen gas is fed to the engine changing pressure into mechanical power. The only exhaust is nitrogen. The usage of cryogenic fuels has sustainable benefit over other fuel. Also, factors such as production and storage of nitrogen and pollutants in the Exhaust give advantage for the cryogenic fuels.*

**Keywords -Difficulties in implementation, Efficiency, Performance of Cryocar, Rankine Cycle.**

## I. INTRODUCTION

As the world progresses through the 21st century, it causes increasing fuel prices, tougher emissions regulations, and a switch on renewable energy sources. These consequences are evident in the increased accessibility of extreme low emissions gas vehicles and gas-electric hybrids. The main disadvantage of both of these advancements is that they are yet dependent on fossil fuel and that they produce harmful emissions, even though in smaller amounts. So alternative fuel research has been increased, focusing on H<sub>2</sub> and fuel-cell technology. [1] Liquid N<sub>2</sub> is one of best possible alternative energy carrier, as it can be cheaply produced, is non-flammable, produces only the emission of N<sub>2</sub> back into the environment, and is renewable. Heat exchangers convert liquidN<sub>2</sub> into gas up to ambient temperature, and also provide the needed pressure to power for actuation system. This heating is done by the atmosphere without any additional heat sources, resulting in an easy, authentic, and potentially effective propulsion system. When the only heat input to the engine is supplied by atm. heat exchangers, an automobile can easily be propelled while satisfying stringent tailpipe emission standards. N<sub>2</sub> propulsive systems can provide automotive ranges of nearly 400 km in the zero emission modes, with decreases operating costs than those of the electric cars currently being considered for mass production. In geographical regions that allow ultra low exhaust vehicles, the range and performance of the liquid N<sub>2</sub>automobile can be fundamentally extended by the accession of a small efficient burner. Some of the advantages of a transportation

infrastructure based on liquid  $N_2$  are that recharging the energy storage system only requires minutes and there are minimal environmental hazards associated with the manufacture and use of the cryogenic "fuel". The basic idea of  $N_2$  propulsion system is to utilize the atmosphere as the heat source.

## **II. FACTORS EFFECTING CRYOCARS EFFICIENCY**

### **2.1 Cost Of Production**

Liquid  $N_2$  production is an energy-intensive process. Currently practical refrigeration plants producing a few tons/day of liquid  $N_2$  operate at about 50% of Carnot efficiency.

### **2.2 Energy Density Of Liquid $N_2$**

Any process that relies on a state change of a substance will have much lower energy densities than processes involving a chemical reaction in a substance, turns have less energy density than nuclear reactions. The energy density derived from  $N_2$ 's isobaric heat of evaporation and  $C_p$  (specific heat) in gaseous state that can be realized from liquid  $N_2$  at atm. pressure and  $0^\circ C$  ambient temperature is about 97 W-hr/kg. This compares with about 3,000 W-hr/kg for a gasoline combustion engine running at 28 percent thermal efficiency & 30 times the density of liquid  $N_2$  used at the Carnot efficiency.

For an constant heat expansion engine to have a range comparable to an I.C. (internal combustion) engine, a 350-litre (92 US gal) isolated onboard storage vessel is required. A practical volume, but a noticeable increase over the typical 50-litre (13 US gal) gasoline tank.

### **2.3 Frost Formation**

Unlike I.C. engines, using a cryogenic working fluid requires heat exchangers to heat and cool the working fluid. In a humid atmosphere, ice formation will block heat flow and thus represents an engineering challenge. To prevent ice build up, multiple working fluids can be used. This adds topping cycles to ensure the heat exchanger does not come below  $0^\circ C$ . Additional heat exchangers, weight, complexity, efficiency loss, and expense, would be required to enable ice free operation.

### **2.4 SAFETY**

However efficient the insulation on the  $N_2$  fuel tank, there will be fatal losses by evaporation to the environment. If a vehicle is stored in a poorly ventilated space, there is some risk that leaking  $N_2$  could reduce the  $O_2$  concentration in the air and cause asphyxiation. Since  $N_2$  is a colourless and odourless gas that already makes up 78 % of air, such a change would be difficult to detect. Cryogenic liquids are hazardous if spilled. Liquid  $N_2$  can cause frostbite and can make some materials extremely brittle. As liquid  $N_2$  is colder than  $90.2K$ ,  $O_2$  from the atmosphere can condense. Liquid  $O_2$  can spontaneously and violently react with organic chemicals, including fossil fuel products like asphalt since the liquid to gas expansion ratio of this substance is **1:694**, a enormous amount of force can be generated if liquid  $N_2$  is rapidly vaporized. In an accident in 2006 at Texas A&M University, the pressure-relief valve of a tank of liquid  $N_2$  were sealed with brass Plugs. As a result, the tank failed catastrophically, and blasted. This cause difficulty in implementation.



### 2.5 Tank

The tanks must be designed to safety standards befitting for a pressure vessel, such as ISO 11439. The storage vessel may be made of: Steel, Al, Carbon fibre, Kevlar, other materials or combinations of the above. The fibres materials has considerably low density than metals but generally more costly. Metal tanks are corrosive but it can withstand more number of pressure cycles.

### 2.6 Material For Air Motor / Double Rod Piston Cylinder

As LN<sub>2</sub> is at cryogenic temperature it is difficult to use normal material in expander / motor as it get brittle it & produces stresses. So material used for it should be properly selected as per their properties to withstand such low temperature.

**Table 1: Liquefaction temperatures for some systems [2]**

System	CH <sub>4</sub>	O <sub>2</sub>	Ar	CO <sub>2</sub>	N <sub>2</sub>	Ne	H <sub>2</sub>	He
Liquefaction temperature(K)	111.7	90.1	87.4	81.1	77.3	27.2	20.4	4.2

For cryogenics applications, materials must be carefully selected because of the forcefully changes in the properties of materials at low temperature. Materials which are normally ductile at atm. temperature may become extremely brittle subjected to cryogenic temperature, while some improves ductility. Once the materials are selected, the method of Joining them must carefully consider to insure that the desired performance is conserve by using the proper bonding, brazing, or welding techniques and materials although at low Temp. strength and stiffness of most materials increase, they tend to reduce in size and become rather brittle. Heating solid body from absolute zero requires energy. In a free body, this energy apparent itself in two ways: an increase in temperature and a change in volume. Both of these are directly related to the additional vibration energy of the individual Atoms. [2]

### III. WORKING

It works on simple thermodynamic Rankine Cycle:

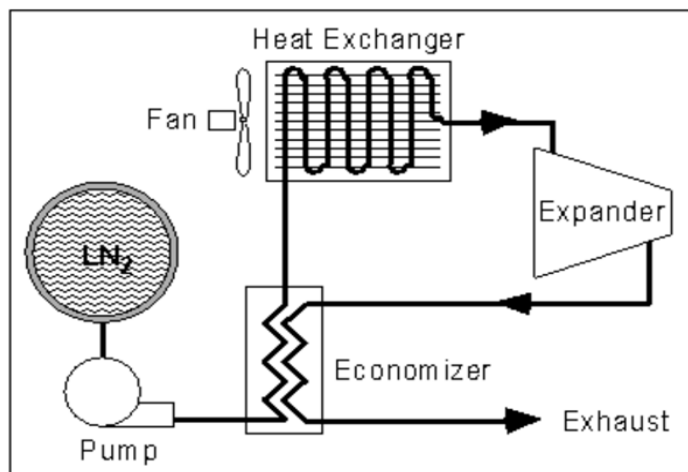


Fig1: LN<sub>2</sub> liquid N<sub>2</sub> propulsion cycle. [3]

### 3.1 Parts of a Liquid N<sub>2</sub> Propulsion Cycle

The main parts and their functions are discussed in detail as follows:

#### 3.1.1 Cryogen Storage Vessel

The primary design constraints for automobile cryogen storage vessels are resistance to deceleration forces in the horizontal plane in the event of traffic accident, low boil-off rate, small size and mass and reasonable price. Crash-worthy cryogen vessels are being developed for hydrogen-fuelled vehicles that will avoid loss of insulating vacuum at closing speeds of over 120 km/h. Moderately high vacuum (10<sup>-4</sup> torr) with critical insulation can provide boil-off rates as low as 1.5% per day in 200 litre (53 gal) containers. Using appropriate titanium or Al alloys for the inner and outer vessels, a structurally reinforced Dewar could readily have a seven-day holding period. The cost of a mass produced 200 litre automotive tanks for liquid hydrogen containment has been estimated to be between \$200 and \$500 (in 1990 dollars). Thus the expense of a 400 litre LN<sub>2</sub> tank (or two 200 litre tanks) is expected to be reasonable. [3]

#### 3.1.2 Pump

The pump is used to pump the liquid N<sub>2</sub> into the engine. The pumps used for this purpose have an operating pressure ranging between 480 –580 Psi. As the pump, sucks liquid instead of gas, it is noticed that the efficiency is high. [5]

#### 3.1.3 Economizer

A preheater, called an economizer, uses leftover heat in the engines exhaust to preheat the liquid N<sub>2</sub> before it enters the heat exchanger. Hence it acts as a heat exchanger between the incoming liquid N<sub>2</sub> and the expel gas which is left out. This is similar to the preheating process which is done in compressors. As the use of the economizer, the efficiency is improved considerably. The design of this heat exchanger is such as to avoid frost formation on its outer surfaces. It will also increase performance of car.

#### 3.1.4 Expander

The maximum work output of the LN<sub>2</sub> engine results from an isothermal expansion stroke. Vehicle power and torque demands would be satisfied by both choking the mass flow of LN<sub>2</sub> and by controlling the cut-off point of N<sub>2</sub> injection, which is similar to how traditional reciprocating steam engines are regulated. The maximum power

output of the propulsion engine is limited by the highest rate at which heat can be absorbed from the environment. The required control system to accommodate the desired vehicle performance can be effectively implemented with either manual controls or an on-board computer. The transient responses of LN<sub>2</sub> power plant and corresponding operating procedures are topics to be investigated. [3]

### 3.1.5 Heat Exchanger [1]

The primary heat exchanger is a critical component of a LN<sub>2</sub> car. For a constant heat expansion engine having an injection pressure of 5 MPa, the heat absorbed from the environment can, in principle, be converted to useful mechanical power with about 45% efficiency. Thus the heat exchanger system should be provisionally designed to absorb at least 76 kW from the environment when its temperature is about 0°C. To estimate the volume and mass of the primary heat exchanger, it was modelled as an array of individually fed tube elements that pass the LN<sub>2</sub> at its extreme discharge without excessive pressure drop. Each element is a 10 m long section of Al tubing having an outside diameter of 10 mm and a wall thickness of 1 mm.

The exterior heat transfer coefficient is based on that for cylinder in cross flow and the internal heat transfer is for fully developed agitated flow. The bulk temperature of air is assumed to decrease across each tube row as determined from energy conservation and the pressure drop is determined for the whole tube bank. The heat transfer calculations account for N<sub>2</sub> pressure drop and variations in its thermal properties in the tube elements. Some of the significant phenomena not considered at this stage of analysis were the effects of the transient LN<sub>2</sub> flow rates, start up, ice accumulation, tube fins, and axial thermal conduction.

The formation of prime ice is so highly probable. The atm. moisture will be removed relatively quickly as the ambient air is chilled over the first few tube rows, leaving enormously dry air to warm up the colder parts at the rear of the heat exchanger where the LN<sub>2</sub> enters. Surface coatings such as Teflon can be used to prevent unwanted ice build-up and active measures for vibrating the tube elements may also be applied. However, these approaches may not be necessary since high LN<sub>2</sub> flow rates are also wanted during times of peak power necessity and the heat exchanger elements are much longer than essential to elevate the LN<sub>2</sub> temperature to near atmospheric at the lower flow rates required for cruise. Thus, the frosted tube rows may have ample opportunity to de-frost once the vehicle comes up to speed.

Even though inclement weather will certainly demean the performance of the cryomobile, it will not forbid effective operation. If the propulsion system operating circumstances were such that the LN<sub>2</sub> could only be heated to 270 K prior to injection, the flow rates of LN<sub>2</sub> for the adiabatic and isothermal cycles to generate 35 kW would be 120 gm/sec and 187 gm/sec, respectively. The antecedent described heat exchanger configuration can theoretically heat the higher LN<sub>2</sub> flow rate to 260 K with 25 radiator elements when the vehicle is travelling at 25 km/sec (18 mi/h) and the ambient air temperature is only 0°C. The LN<sub>2</sub> pressure drop would be about 0.055 MPa, which is easily compensated for with the cryogenic pump. The electric fan would require around 1.5 kW to accelerate the air and overcome the 400 Pascal pressure drop through the heat exchanger if the vehicle were standing still. Since each element is 0.80 kg, the total tubing mass would be 19 kg. If the same mass was added by the duct and manifolds then the total mass of the heat exchanger would be less than 40 kg. When operating on a typical California day, it is expected that this over-designed cryogen vaporizer will readily heat the LN<sub>2</sub> up to ambient temperature without any appreciable icing.

#### IV. POWER CYCLE

There are many thermodynamic cycles available for utilizing the thermal potential of liquid  $N_2$ . This system uses an open Rankine cycle. The temperature versus entropy diagram for the open Rankine cycle is described below.

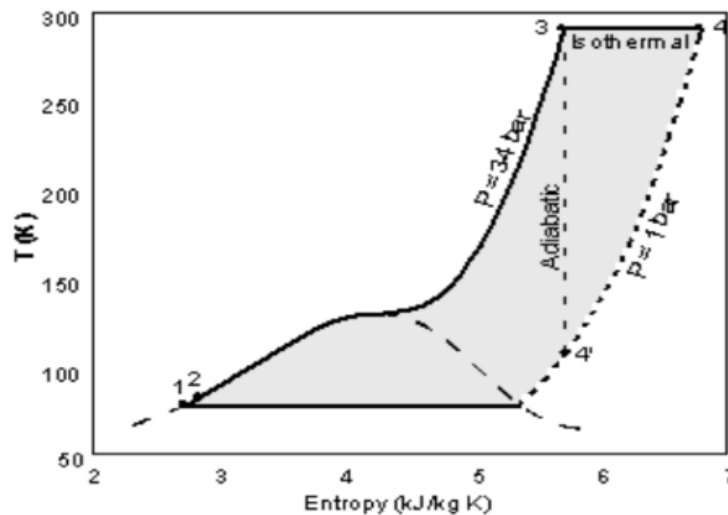


Fig2: Temperature - entropy diagram for the open Rankine cycle. [3]

State 1 is the cryogenic liquid in storage at 0.10 MPa and 77 K. The liquid is pumped up to system pressure of 5 MPa (supercritical) at state 2 and then enters the economizer. State 3 indicates  $N_2$  properties after it is being preheated by the exhaust gas. Further heat exchange with atmospheric air brings the  $N_2$  to 290 K at state 4, ready for expansion. Isothermal expansion to 0.2 MPa at state 5 would result in the  $N_2$  exhaust having sufficient enthalpy to heat the  $LN_2$  to above its critical temperature in the economizer, whereas adiabatic expansion to state 6 would not leave enough enthalpy to justify its use. The specific work output would be 300 and 200 kJ/kg- $LN_2$  for these isothermal and adiabatic cycles, respectively, without considering pump work. While these power cycles do not make the best use of the thermal potential of the  $LN_2$ , they do provide specific energies competitive with those of batteries.

#### 4.1 Performance of the open Rankine cycle

The thermodynamic and economic performances of the isothermal and adiabatic modes of the open Rankine cycle are shown in Table 1. These figures are based on the specifications of a modified Honda CRX for which performance data were available. The cost of 3 ¢ per kg- $LN_2$  was derived assuming only the energy cost of production.

**Table 2: Performance of the open Rankine cycle [1]**

Process	Adiabatic	Isothermal
Pump work	6 KJ/Kg-LN <sub>2</sub>	6 KJ/Kg-LN <sub>2</sub>
Net output	194 KJ/Kg-LN <sub>2</sub>	314 KJ/Kg-LN <sub>2</sub>
Heat input	419 KJ/Kg-LN <sub>2</sub>	750 KJ/Kg-LN <sub>2</sub>
Energy density	54 W-h/Kg-LN <sub>2</sub>	87 W-h/Kg-LN <sub>2</sub>
LN <sub>2</sub> flow rate	1.5 Kg/Km	0.93 Kg/Km
Operating cost	3.9 Rs/km	2.4 Rs/Km

### V. ADVANTAGES

- Studies indicate that liquid N<sub>2</sub> automobiles will have significant performance and environmental advantages over electric vehicles.[1]
- A liquid N<sub>2</sub> car with a 60 gallon volume tank will have a potential range of up to 200 miles, or twice than that of a typical electric car. Furthermore, a liquid N<sub>2</sub> car will be much lighter and refilling its tank will take only 10-20 minutes, rather than the several hours required by most electrical car concepts.
- Motorists will fuel up at filling stations likely to today’s gasoline stations. When liquid N<sub>2</sub> is manufactured in large quantities, the operating cost per mile of a liquid N<sub>2</sub>car will not only be less than that of an electric car but will actually be competitive with that of a gasoline car.
- Economical: LO<sub>x</sub>& LH<sub>2</sub> costs less than gasoline.[5]

### VI. DISADVANTAGES

- The principledrawback is the inefficient use of primary energy. Energy is used toliquidify N<sub>2</sub>; turn provides the energy to run the motor. Any conversion ofenergy between forms results in loss. For liquid N<sub>2</sub> cars, energy lost whenelectrical energy is converted to liquid N<sub>2</sub>.
- Liquid N<sub>2</sub> is not yet available in public refuelling stations.
- Leakage.[6]
- Boil off rate.[5]

### VII. FUTURE SCOPE

- Range Extension and Power Boosting :

Range extension and performance enhancement can be complete by heating the liquid nitrogen to above ambient temperatures with the combustion of a relatively low contamination fuel such as ethanol or natural gas. By increasing the gaseous nitrogen temperature to 500 K, the specific work at 5 MPa for the adiabatic engine is increased by 60.75% to make it nearly the same as the work from aconstant heat expansion engine operating at 300 K. In this particular propulsive cycle an extra heat addition of up to 200°C results in only a 30% increase in limited power. Thus the advantage of operating above atm. temperature depends, in part, on how constant heat

the expansion process can be made to be. There is also the provocative possibility of storing energy for boosting power or wider range by applying a medium that undergoes a state change to the final super heater section of the heat exchanger system. Ideally the state change material would be slowly “recharged” as it imbibes heat from the environment while the vehicle is parked and during cruise when peaking power is not required. Fast recharging with electric heaters may also be considered. We recognize that this added ramification must compete in mass and concentrated with the secondary of just carrying more LN<sub>2</sub>.

### **VIII. CONCLUSION**

The advantage for utilizing the available energy of liquid N<sub>2</sub> for automotive propulsion looks much guaranteed. Time to refuel, infrastructure investment, and economical are among the issues to consider, in added the range and performance, when comparing the relative merits of different zero emission vehicle technologies. The convenience of pumping a fluid into the storage vessel is very attractive when compared with the typical recharge times colligate with lead-acid batteries. Manufacturing LN<sub>2</sub> from atm. air inherently removes small quantities of atm. pollutants and the installation of largescale liquefaction device at existing fossil-fuel power stations could make flue gas condensation processes economical and even discard the exhaust of CO<sub>2</sub>.

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