

# COMPARATIVE STUDY OF ANALYSIS ON MASONRY INFILL WALLS

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## ABSTRACT

*It is common misconception that masonry infill in structural steel or reinforced concrete frames can only increase the overall lateral load capacity, and therefore must always be beneficial to seismic performance. If the masonry infill is ignored in the design phase, it may be assumed that each frame in each direction is subjected to very similar seismic lateral forces, because of the structural symmetry. The true influence of the infill on frames will be to stiffen these frames relative to the other frames. The consequence will be that the natural period of the structure will decrease, and seismic forces will correspondingly increase. Further the proportion of the total seismic shear transmitted by the infilled frames will increase because of the increased stiffness of these frames relative to the other frames. The high shear forces generated in the infilled frames are transmitted primarily by shear stresses in the panels.*

*The aim of this research work is to present a comparatively study and seismic analysis of multi storey 3D-RC frame building with infill and without infill for seven storey building using STAAD-PRO. The modal analysis of structure is carried out to know whether stiffness and mass of structure is correct or not.*

**Keywords --** *Masonry Infill Frame, STADD-Pro, Model Analysis, Displacement At Various Node*

## I INTRODUCTION

Masonry infills work as compressive strut, infills have more significant in lateral loads such as seismic and wind forces as compared to vertical loads. The masonry walls used for partition purpose in buildings will contribute to initial lateral stiffness significantly. In severe earthquake loading the walls will get cracked and contribution to lateral stiffness is negligible. Masonry walls can be modeled as diagonal strut model or continuum plate model. The foregoing considerations will often mitigate against the use of isolated panels, and the subsequent discussion will be limited to interacting structural infill, where the role of the infill in influencing stiffness and strength is fully considered in the design process. In this work, STADD Pro software has been used in order to analyze and design RCC frame structure (G+6)

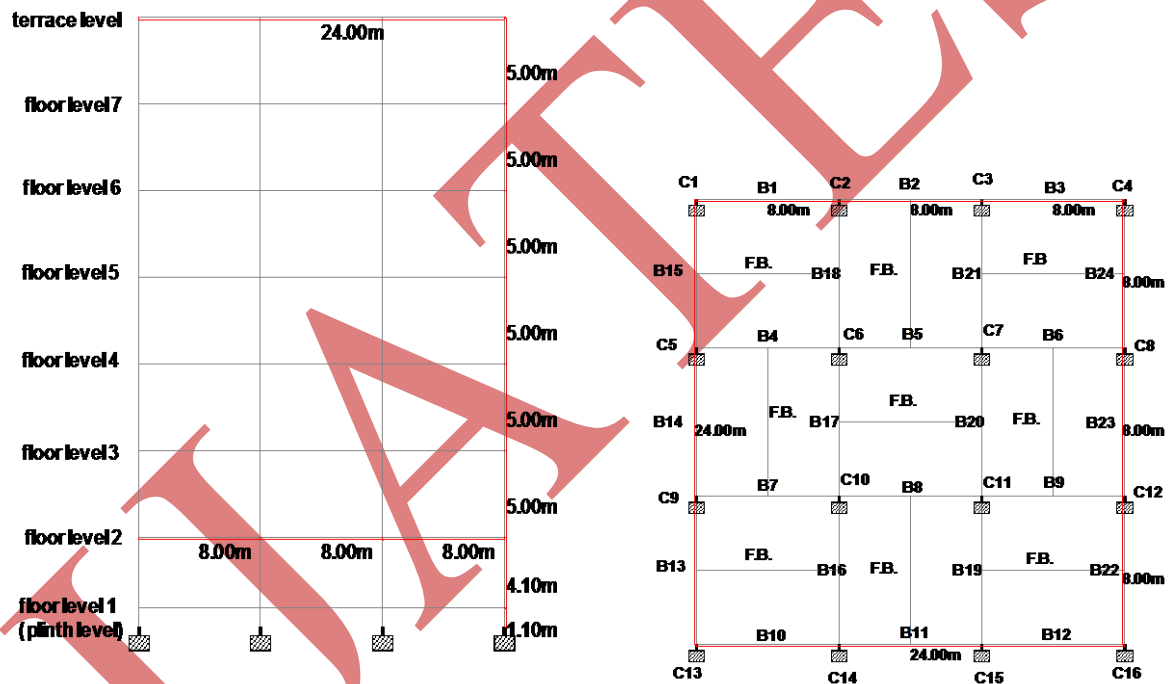
## II STATEMENT OF PROBLEM

A (24×24)m , G+6 building with regular structure for a commercial complex is considered for study . modeling, analysis and design of structure is done on STADD Pro software. The building will be used for exhibitions as a show room, so that there are no inside walls in the building. Only external wall 230 mm thick with 12 mm plaster on both sides are considered.

**Table 1** Preliminary Data

|                              |              |
|------------------------------|--------------|
| length×width                 | (24×24)m     |
| No. of storey                | 7            |
| Beam (at all floors)         | (300×600 )mm |
| Ground Beam                  | (300×600) mm |
| Column(at all typical floor) | (500×500)mm  |
| Column (below ground level)  | (950×950)mm  |
| Slab thickness               | 100mm        |
| Support conditions           | Fixed        |
| Beam releases                | Axial force  |

## 2.1 Loading considerations



**Fig. 1**

Loads acting on the structure are dead load(DL), live load(IL) and earthquake load(EL).

DL: self weight of the structure, floor load and wall loads.

- Live load : 4.0 kN/m<sup>2</sup> at floor level, 1.0 kN/m<sup>2</sup> on terrace level
- Floor finish : 1.0 kN/m<sup>2</sup>
- Water proofing : 2.0 kN/m<sup>2</sup>
- Floor finishes : 1.0kN/m<sup>2</sup>
- Seismic zones : IV
- Location : Gorakhpur city
- Soil type :Hard soil

- Response reduction factor :5
- Importance factor :1.5
- Damping : 5%
- Time period : 0.6466 (calculated as per IS 1893:2002)
- Wind load : As per IS: 875 ( not considered wind load for design because of Earthquake loads exceed the wind loads , it exceed once a time Over 500 years.)
- Earthquake load : As per IS -1893-2002

## 2.2 Load Combinations

The analysis has been carried out for Dead load (DL) , Live load or imposed load (IL) and earthquake load (EL) in both the direction i.e. sway to left (+ EL) and sway to right (-EL) by a Stadd- Pro.

The combination of the above cases has been made according to Clause 6.3 of IS 1893(Part 1) : 2002. the maximum moments and forces for the beams and columns for all the load combinations for each member are considered for the design.

The different load combinations are:

1. 1.5(DL+IL)
2. 1.2(DL+IL+ELx)
3. 1.2(DL+IL-ELx)
4. 1.2(DL+IL+ELz)
5. 1.2(DL+IL-ELz)
6. 1.5(DL+ELx)
7. 1.5(DL-ELx)
8. 1.5(DL +ELz)
9. 1.5(DL – ELz)
10. 0.9 DL+1.5 EL
11. 0.9 DL–1.5 EL

## III. BUILDING CONFIGURATION OF 7 STOREY BUILDINGS FOR ANALYSIS WITH DIFFERENT % OF MASONRY INFILL WALLS

In this work, Five models were used to differentiate the effect of infill walls and location of infill on building analysis and effect of infill walls on lateral resistance and capacity of building is studied and compared with bare frame.

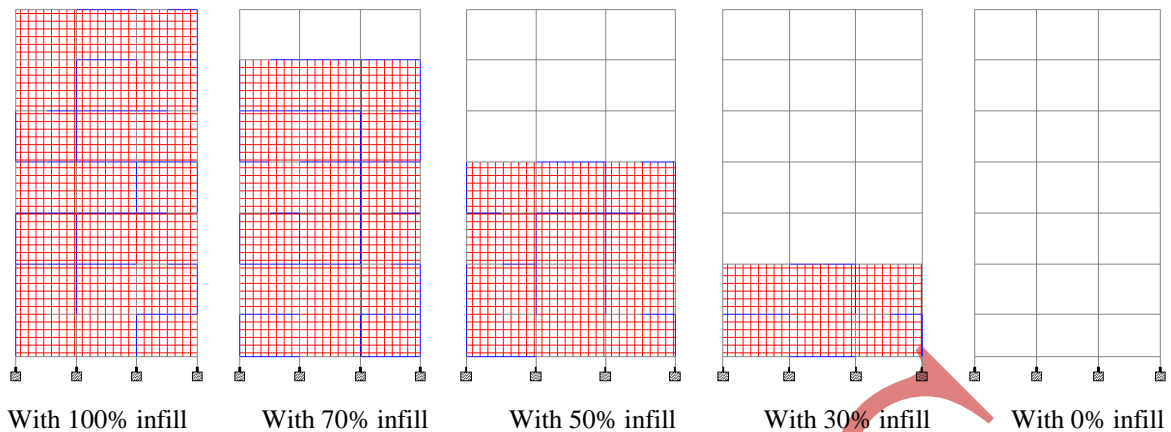


Fig. 2

#### IV. COMPARATIVE RESULTS

##### 4.1 Modal Analysis of 3D Frame

The modal analysis of structure is carried out to know whether stiffness and mass of structure is correct or not. The mass of structure is calculated from dead load and 50% of live load. As the structure is symmetrical, the mass of each member is lumped at respective ends. Since the structure is unsymmetrical in mass and stiffness the fundamental mode is torsion mode with time period.

Table 2 Result of modal analysis

| % of infill | Mode No. | TimePeriod (Sec) | Modal mass participation(%) |      |       |
|-------------|----------|------------------|-----------------------------|------|-------|
|             |          |                  | X                           | Y    | Z     |
| With 100%   | 1        | 0.32444          | 63.37                       | 0.00 | 18.08 |
|             | 2        | 0.32410          | 18.09                       | 0.00 | 63.41 |
|             | 3        | 0.18073          | 0.00                        | 0.00 | 0.00  |
| With 70%    | 1        | 0.50881          | 8.94                        | 0.00 | 19.24 |
|             | 2        | 0.50866          | 19.26                       | 0.00 | 8.91  |
|             | 3        | 0.42372          | 0.00                        | 0.00 | 0.00  |
| With 50%    | 1        | 1.26501          | 0.00                        | 0.00 | 35.54 |
|             | 2        | 1.26142          | 35.59                       | 0.00 | 0.00  |
|             | 3        | 1.09912          | 0.00                        | 0.00 | 0.00  |
| With 30%    | 1        | 2.05730          | 0.00                        | 0.00 | 54.41 |
|             | 2        | 2.05005          | 54.45                       | 0.00 | 0.00  |
|             | 3        | 1.79430          | 0.00                        | 0.00 | 0.00  |
| With 0%     | 1        | 2.72276          | 0.00                        | 0.00 | 71.71 |
|             | 2        | 2.71148          | 71.72                       | 0.00 | 0.00  |
|             | 3        | 2.38509          | 0.00                        | 0.00 | 0.00  |

**4.2 Relative displacement of storey for following infills at different node**

**Table 3 (In X direction)**

| Infill /Node | 1 | 2      | 3       | 4       | 5       | 6        | 7        | 8        | 9        |
|--------------|---|--------|---------|---------|---------|----------|----------|----------|----------|
| With 100%    | 0 | 5.516  | 12.031  | 16.572  | 20.721  | 24.514   | 27.951   | 31.053   | 34.06    |
| With 70%     | 0 | 5.511  | 12.022  | 16.573  | 20.739  | 24.588   | 28.103   | 32.72    | 87.98    |
| With 50%     | 0 | 5.485  | 11.995  | 16.69   | 20.907  | 29.015   | 226.498  | 401.984  | 495.853  |
| With 30%     | 0 | 5.508  | 11.762  | 23.308  | 368.791 | 731.287  | 1011.547 | 1198.691 | 1296.317 |
| With 0%      | 0 | 14.503 | 322.853 | 848.693 | 1317.61 | 1696.431 | 1981     | 2170.995 | 2271.36  |

**Table 4 (In Y direction)**

| Infill /Node | 1 | 2     | 3      | 4      | 5      | 6      | 7      | 8      | 9      |
|--------------|---|-------|--------|--------|--------|--------|--------|--------|--------|
| With 100%    | 0 | 2.592 | 7.744  | 10.067 | 11.102 | 11.59  | 11.784 | 11.848 | 11.94  |
| With 70%     | 0 | 2.603 | 7.79   | 10.151 | 11.251 | 11.867 | 12.306 | 12.976 | 13.215 |
| With 50%     | 0 | 2.681 | 8.114  | 10.791 | 12.536 | 15.193 | 17.422 | 18.478 | 18.784 |
| With 30%     | 0 | 2.929 | 9.457  | 15.79  | 22.181 | 26.369 | 28.717 | 29.762 | 30.055 |
| With 0%      | 0 | 2.057 | 12.319 | 21.939 | 28.628 | 32.883 | 35.261 | 36.323 | 36.621 |

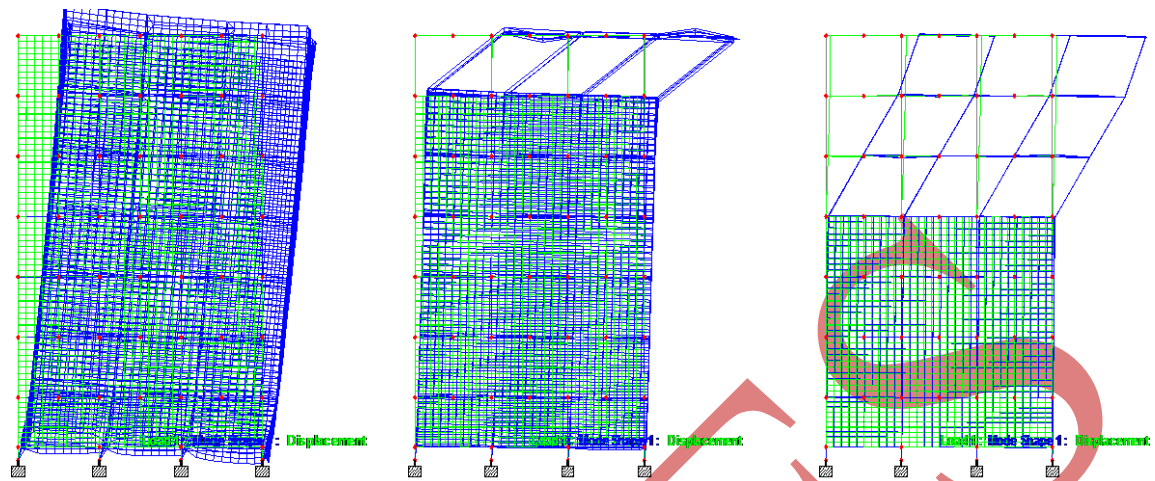
**Table 5 (In Z direction)**

| Infill /Node | 1 | 2      | 3       | 4       | 5        | 6        | 7        | 8        | 9        |
|--------------|---|--------|---------|---------|----------|----------|----------|----------|----------|
| With 100%    | 0 | 5.518  | 11.955  | 16.531  | 20.688   | 24.482   | 27.92    | 31.026   | 34.01    |
| With 70%     | 0 | 5.512  | 11.945  | 16.53   | 20.704   | 24.554   | 28.098   | 32.532   | 88.086   |
| With 50%     | 0 | 5.483  | 11.911  | 16.637  | 20.947   | 28.494   | 227.027  | 404.052  | 498.866  |
| With 30%     | 0 | 5.485  | 11.801  | 22.388  | 369.891  | 735.615  | 1018.404 | 1207.188 | 1305.673 |
| With 0%      | 0 | 14.497 | 324.746 | 855.112 | 1328.336 | 1710.586 | 1997.616 | 2189.112 | 2290.176 |

**Table 6 (Resultant)**

| Infill /Node | 1 | 2      | 3       | 4       | 5        | 6        | 7        | 8        | 9        |
|--------------|---|--------|---------|---------|----------|----------|----------|----------|----------|
| With 100%    | 0 | 8.221  | 18.644  | 25.48   | 31.314   | 36.533   | 41.226   | 45.467   | 49.591   |
| With 70%     | 0 | 8.217  | 18.652  | 25.514  | 31.39    | 36.718   | 41.601   | 47.93    | 125.197  |
| With 50%     | 0 | 8.206  | 18.751  | 25.919  | 32.141   | 43.412   | 321.163  | 570.255  | 703.626  |
| With 30%     | 0 | 8.307  | 19.158  | 35.969  | 522.798  | 1037.596 | 1435.688 | 1701.484 | 1840.142 |
| With 0%      | 0 | 20.609 | 458.089 | 1204.98 | 1871.201 | 2409.37  | 2813.552 | 3083.302 | 3225.729 |

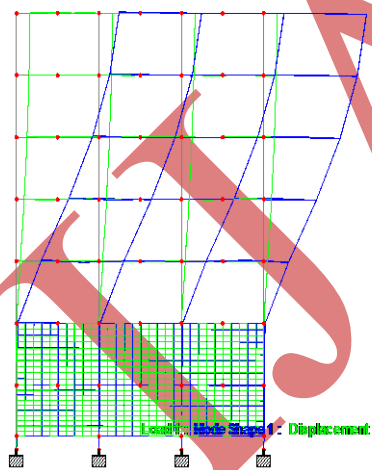
### 4.3 Displacement and Mode shape of comparative infills



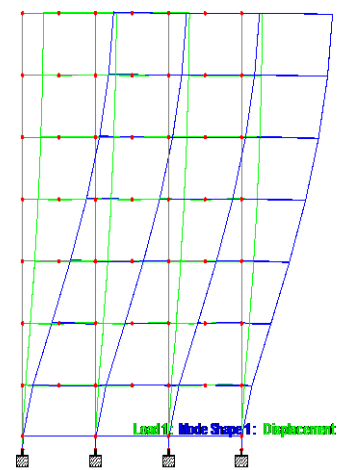
With 100% infill

with 70% infill

with 50% infill



With 30% infill



with 0% infill

Fig. 3

#### 4.4 Roof displacement ( at node 9)

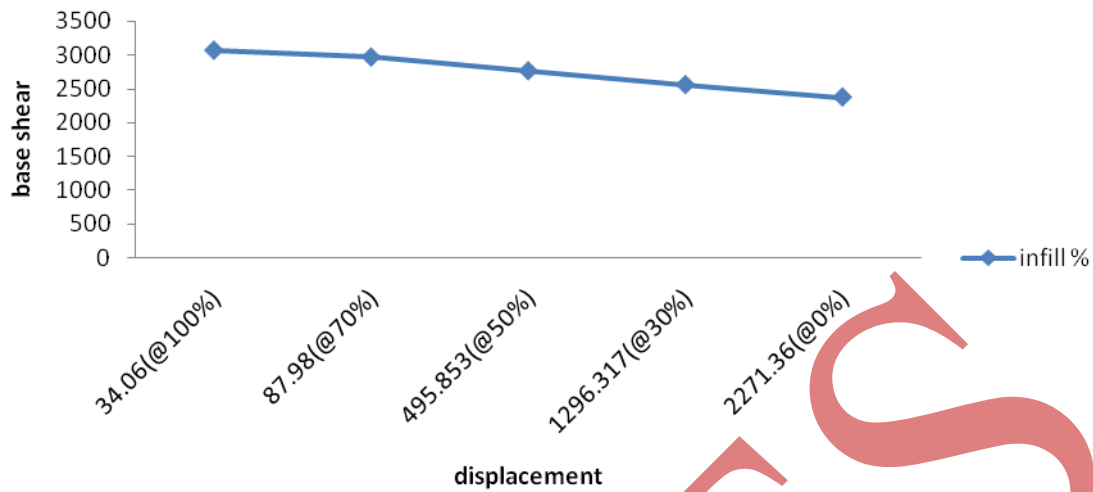


Fig. 4

#### V. CONCLUSION

From the results, we obtained that masonry infill affects the building displacement at various node due to lateral loads ( seismic ), we may conclude that with 100% infill gave lesser displacement as compared to 70%, 50%, 30% and 0% infills and 100 % infills provides more stiffness relative to other infills. The consequence will be that the natural period of the structure will decrease in 100% infill.

#### VI. REFERENCES

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